



**An exercise which looks funny but which is not and rises questions**

**A Not so easy simple Task**

→ **Come Back to Basics**

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**Far Side - Near Side – Dark Side**

- n Moon side facing the Earth is the **near side**, & the opposite side the **far side**.
- n Far side should not be confused with Dark side, the hemisphere that is not being illuminated by **Sun** at a given moment
- n The day on the Moon last 27.3 earth days

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**What makes the difference on the Moon?**

- n **Lower Gravity: 1/6 of earth value**
  - ☐ G is only 1.62m/sec<sup>2</sup>
  - ☐ Lower weights but same mass
  - ☐ Buoyancy effect is reduced
- n **Different Temperatures**
  - ☐ Sunlit side : ~110°C
    - Water is boiling (enhanced by low atmosphere pressure)
    - Expected problems with electrical equipment
    - Could be decrease by shelter but T closer to dark side
  - ☐ Dark Side : ~-170°C
    - Water is solid
    - Beware of Steel brittleness

.....Don't forget that the near side (facing the earth) and the far side (never seen from the earth) are both exposed to sun at a given moment

- Beware of Strong thermal expansion

**What makes the difference on the Moon?**

- n **No atmosphere:**
  - ☐ Pressure only 10<sup>-12</sup> bar (day) 10<sup>-15</sup> bar (night)
  - ☐ Just a few He(20%), Ne(23%), H<sub>2</sub>(17%) and Ar(16%vol)
  - ☐ Heat transfer by Convection cannot be used
  - ☐ Very low Oxygen (exact level not well known)
    - No combustion possible
    - No Fe oxidation
- n **Low Pressure**
  - ☐ Impact on fluid mechanics of gas knife
  - ☐ Oil, Water, Zn evaporate easily
- n **Cosmic Radiation**
- n **Direct Radiation from Sun**
  - ☐ Equipment will be hit by high energy particle

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**A Limited analysis**

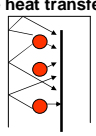
**Whereas Hot Dip Galvanizing include many different processes, only some of them are addressed**

- n Incoming Coils
- n Cleaning
- n Annealing & surface preparation
- n Zinc Coating
- n Final Cooling
- n SKP
- n Oil
- n Defects
- n Operators
- n Energy

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### cmi Annealing

- n No change in the target peak T
- n Combustion is too expensive due to no O<sub>2</sub>
- n Electric heating is easy
  - ☑ Photo cells for electricity production
  - ☑ Radiative heating by Resistance
  - ☑ Furnace casing required to improve radiative heat transfer
    - Use of reflection
    - But the casing may be open
- ... or possible use of Resistance with integrated reflector like UV or IR baking
- ☑ No Heat loss by natural cooling
- n Induction with longitudinal flux limited to ~650°C
- ☑ Use of Transverse flux OK, but edge management is not easy
- n No need of protective atmosphere against oxidation



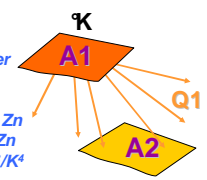
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### cmi The Basics of Radiative Heat transfer

- n Exchange between 2 surfaces
  - ☑ Heat exchanged by A1

$$Q_{12} = A_1 * \epsilon * c_0 * F_{12} * (TK_1^4 - TK_2^4)$$

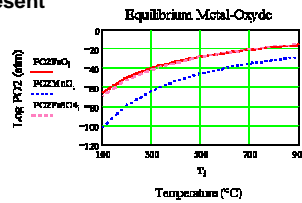
- ☑ With
  - F = shape factor: good in cooling tower
  - A1 = emitting surface
  - T = Temperature: quite low after Pot
  - ε = surface emissivity: ~0.05 for liquid Zn  
~0.12 for solid Zn
  - C<sub>0</sub> = Boltzman Constant: 5.67E-8 W/m<sup>2</sup>/K<sup>4</sup>



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### cmi Surface Preparation

- n No need of H<sub>2</sub> for reduction... if cold rolled on the moon
- ☑ Not so clear if rolled on the earth: 100nm oxide-hydroxide present



- ☑ PO<sub>2</sub> < 10<sup>-60</sup> at 500°C to FeO -> Fe + 1/2 O<sub>2</sub>
- ☑ If P<sub>moon</sub> = 10<sup>-15</sup>, Oxygen concentration is low
  - Maybe low PO<sub>2</sub> reached
  - High T<sup>o</sup> will help kinetics of spontaneous reduction

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### cmi Surface preparation

- n Strictly: No need of N<sub>2</sub> for protective gas
- ☑ No oxidant is present
- n But Surface Segregation will occur by Gibbs Segregation
  - ☑ All elements moving to grain boundary will enrich the surface in Vacuum annealing
    - The Grain boundary is an Oxygen free zone with lots of voids
  - ☑ Risk of Carbon, P, S, Sb, Sn covering the surface
    - Changes of wettability
    - Carbon will help oxide reduction in solid state on High Carbon steel
    - Risk to form spangles in a Pb-Sb free bath
  - ☑ Surface enrichment may change the Fe-Zn reaction

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### cmi Cooling before the Coating

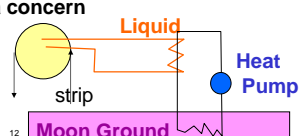
- n Much more difficult because forced convective gas cooling cannot be used
- n Radiative cooling is too slow
- ☑ Strip emissivity is not high: typically 0.2

EqEm 800°C=0.213 Max 15kW/m <sup>2</sup> /side	EqEm 500°C=0.174 Max 13kW/m <sup>2</sup>
➔ 74kW/m <sup>2</sup> /side	➔ 55kW/m <sup>2</sup> /side

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### cmi Cooling before Coating

- n Possibility to use Phase transformation
  - ☑ Liquid evaporation or sublimation on the sheet
    - Ex CO<sub>2</sub> (not available on Moon), Ne...
  - ☑ Need to obtain liquid either by cooling or from earth
  - ☑ Low pressure means spontaneous evaporation of sprays & Drops
- n Re-consider the Roll Quench system
  - ☑ Known that this process induce flatness concerns due to variation of heat transfer with contact force
  - ☑ Cooling the roll is still a concern
    - Gas cooling... H<sub>2</sub>, He
    - Pressurized Water cooling



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### Pressure in the Box & Convection

- Higher Pressure increases Gas consumption
- Low Pressure may impact Heat transfer
- Typically for Forced Convection

$$Nu = f(Re, Pr, Design)$$

$Nu = h * \frac{Dimension}{Conductib}$

$Re = \frac{Velocity * Dimension * \rho}{\mu}$

$Pr = \mu * \frac{Cp}{Conduct}$

- From Practice & Theory
  - $Cp, \mu_{gas}$  and gas conductivity only depends on  $T$ ...except perhaps at very low Pressures
- Correlations  $Nu=f(Re, Pr, Geometry)$  are still valid
  - But keep in mind their validity domain, especially  $Re$

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### Pressure in the Box & Convection

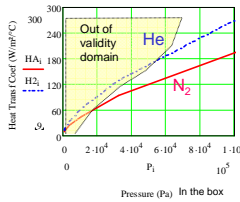
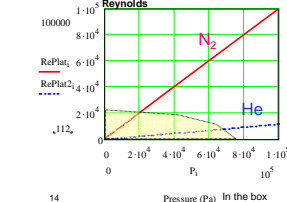
- Effect of Pressure in only on Density
- $Re$  decreases with Pressure

$Nu = h * \frac{Dimension}{Conductib}$

$Re = \frac{Velocity * Dimension * \rho}{\mu}$

$Pr = \mu * \frac{Cp}{Conduct}$

Prediction of h Slot Type: Gap 7mm, Pitch 300mm, Dist 125mm, Gas vel=130m/sec  
Martin Correlations

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### Pressure in Box & Gas Consumption

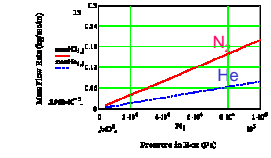
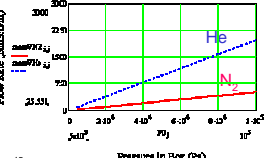
- The Max Gas flow is defined by  $\frac{(\gamma+1)}{2^{(\gamma-1)}}$

$$mMax(\gamma, R, T_{T0}, PP_0) := d \cdot \sqrt{\frac{\gamma}{R \cdot T_{T0}} \cdot PP_0 \left( \frac{2}{\gamma+1} \right)^{\frac{\gamma}{\gamma-1}}}$$

- In kg/sec
- $PP_0, T_{T0}$  = static  $P, T$  in the bow
- $d$  = opening
- $R, \gamma$  = Gas constant

Helium	N2
$\gamma_{He} = 1.65$	$\gamma_{N2} = 1.4$
$R_{He} = 2079$	$R_{N2} = 296.8$

Example Opening 1mm, gas 130°C, 1m width

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### Furnace Design Summary

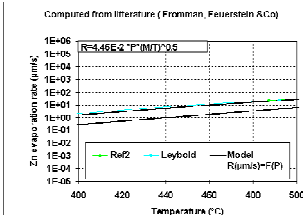
- A furnace under Pressure seems the best
  - Because of cooling
  - To minimize the number of Seals
    - Sonic flow at seals
  - Probably use of He under 0.4atm
    - Available in the environment
    - Good thermal efficiency
    - Risk of Gibbs segregations
- Heat recovery from cooling to obtain heat at the entry
- Electrical heating supplied by Photo cells

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### Zn Pot

- Zn evaporation from the pot is expected Huge
- No Oxide on the surface to impede evaporation
- About 5-10 $\mu$ m/sec at 460°C/sec
  - Explained by the High Vapour Pressure of Zn

But evaporation consume heat: 56J/gr ... reduce T



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### Zn Pot


- 1 $\mu$ m Zn lost/sec: ~7g/m<sup>2</sup>/sec a huge value
- About 1500kg/h for a usual pot (12m<sup>2</sup>, 5 $\mu$ m/sec)
- Consume ~23KWh only for evaporation + 120KWh for heat & melt
- Benefit for the Zn vapour deposition process
- A Nightmare for Zn Yield of Galvanizer
- Dross decantation expected lower
  - Zn viscosity identical
  - Buoyancy force decreased by 6 times
    - 6500-4500 kg/m<sup>3</sup> for Zn & Dross
    - Up force is only 1/6 on the moon
    - The Dross problem is not going to improve
  - Same Fe dissolution
  - Same Zn Viscosity
  - Lower Buoyancy force
  - Higher Fe content in melt

$$V_{dec} = (rFe2Al5)^2 \cdot (\rho_{Zn} - \rho_{Fe2Al5}) \cdot \frac{g}{\mu_{Zn}^2}$$

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### Reaching the Coating Weight

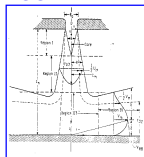
- The Final coating weight is the result of External forces
  - Entrainment by viscosity
    - No change expected
  - Application of external forces
    - Typically P gradient and Shear Forces in Wiping in atmosphere
  - Gravity is predicted to have no effect on the Final coating weight
    - Due to the much higher effect of knife forces



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### Wiping

- Present prediction based on Navier Stokes equations can be used because the Zn layer is continuous
- Any type of Forces can be applied in wiping models
  - Magnetic Wiping never succeeded on earth
    - Heating problems
    - Edges management
- No change expected on the moon
  - Gas Wiping
    - Need full re-analysis because P shape depends on Navier Stokes

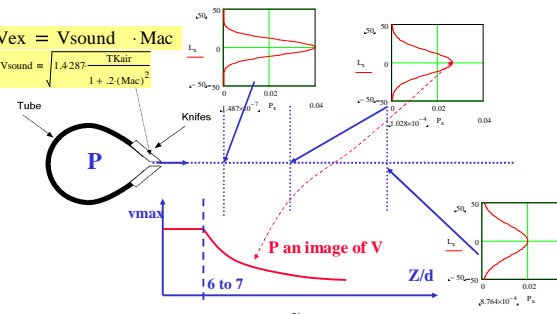


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### Gas Wiping

- In atmosphere, Gas Velocities decrease due to Viscous entrainment

$$V_{ex} = V_{sound} \cdot Mac$$

$$V_{sound} = \sqrt{1.4 \cdot 287 \cdot T_{Kair} / (1 + 0.2 \cdot (Mac)^2)}$$


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### Gas Wiping

- In Vacuum, situations are different
  - No viscous entrainment of ambience

$$P_{Gradient} = BB \cdot \frac{\rho_{gas}}{2} \cdot (V_{gas})^2$$

$$Shear = -CC \cdot \frac{\rho_{gas}}{2} \cdot (V_{gas})^2 \cdot d$$

NOT Valid because gas velocity is no more Gaussian Shape

At nozzle exit

- Exit Velocities are expected much over Sound speed....
  - Shock waves cannot be avoided due to the very low pressure on the moon

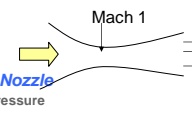
BB, CC= Constant  
d= nozzle opening  
Z= distance

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### Gas Dynamics & Temperature

- Gas speed is defined by the Compressive Expansion Law
  - In Vacuum, the Max velocity is defined by
 
$$V_{max} = \sqrt{\left(\frac{2 \cdot \gamma}{\gamma - 1}\right) \cdot \frac{R}{M} \cdot T_{gas}}$$

M= Molar mass  
R= gas constant
- which correspond to all gas energy transformed into velocity
  - Example:
    - TN<sub>2</sub>=350K Velocity= 852m/sec much higher than sound velocity
  - The Max Velocity requires
    - Perfectly adapted Converging Diverging Nozzle
      - Not possible on the moon due to the very low pressure
      - Shape should be adjusted with Wiping P
      - Not possible to avoid Shock waves



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### Gas jet on the Moon

- The Wiping Force is the Pressure Gradient
  - How does it develop with:
    - A choked gas flow with shock waves
    - An expansion in Vacuum without viscous entrainment coming
- The interaction Gas Liquid Zn must be reanalyzed
  - The Pressures on the sheet must be recomputed
  - Shear stresses are expected very different

# A Whole New World is Coming

- But a Final solution will exist for NOISE
  - No media for Pressure waves transportation

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### And what is the effect of Gravity

- Gravity impacts the total Film Thickness profile under the knives
- But Gravity has no effect of the final coating weight because of high wiping force

**On Earth**

**On the Moon**

### And what is the effect of Gravity

- Explanation**
  - The film thickness at any location is the result of
    - Viscous entrainment
    - External forces
      - Pressure Gradient
      - Shear forces
      - Gravity... constant

Gravity can only impact the film where other forces are low

### And what about Zn Evaporation

- Between Pot and Wiping: No impact**
  - Residence time only 0.2 to 0.15 sec
  - Eventual Zn loss cannot impact the final coating weight
    - Prewiping cannot work
- After wiping is critical**
  - Time in liquid state depends on cooling rate after wiping
  - Typically 6-8sec on a 1mm thickness
    - Loss of 6µm by evaporation (avg 440°C)
    - Much more in practice due to difficulties in cooling
    - Need to adapt coating weight at Nozzle with Solidification time... but thin coating are easy to reach (20g/m² at 180m/min)

Wiping with a Reactive Gas may be mandatory

### Cooling Tower

- The most difficult process**
  - Convection cooling is not possible ... except under atmosphere
- Only radiation is possible**
  - But Zn emissivity is low as well as Temperature
- Not Possible to Cool quickly**
  - Very high tower expected
  - But no vibration induced by cooling
    - No gas impingement
  - Ga has advantage on Gi with a higher emissivity
  - GL will become very critical due to higher T
- Water quench has the same concern**
  - Full evaporation of liquid water due to low Pressure

### The Cooling Tower On the Moon

- Cooling Liquid & Solidified Zn is a nightmare**
  - Zn emissivity cannot be changed
    - No change to increase radiation
  - Make a Closed box with atmosphere???
  - High Tower to increase time.... may be the solution
    - No earthquake
    - No wind
    - Low gravity decrease foundation strength
    - No need of Sidings for the building
      - No sound propagation
      - No dust, no flies and mosquitoes
      - No competitors to watch our process
    - But beware of Sun radiations during day and meteorite drops
    - Beware of strong T-variations inducing Thermal Expansion

### The Cooling Tower

- A possible solution**
  - Closed tower with atmosphere and recover heat on the strip by heat pump (or Peltier cell)
  - Helium could be used for efficiency and avoid Water quench water

**cmr Conclusion**

n **Galvanizing on the Moon is not an easy Task but a good challenge for R&D**

- Ø Cooling is a nightmare
  - In the furnace
  - In the tower
 ...Implying the necessity to work with atmosphere
  - Any finally the use of expensive seals
- Ø Zn Vaporizes Hugely
  - In the Pot
  - After wiping
- Ø Zn Wiping by gas jet must be completely re-analyzed
  - The behaviour of the gas jet is different in Vacuum
- Ø Wet SKP must be analysed

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**cmr And Where on the Moon?**

n **Watch for a Site**

1 of the 2 Photo cell field

Flat and close

In craters may have some advantages  
Less exposed to sun

**cmr Or Where Else?**

n **And what about Venus**

- Ø Strong atmosphere is available
- Ø CO<sub>2</sub> is for Free
- Ø 450°C all the time... lot of energy saving
- Ø 80bar ... good for Zn vaporization

n **But**

- Ø How to avoid Galvannealing .... reaching only a Fe-Zn strip.... Very brittle
- Ø Ageing after SKP cannot be avoided
- Ø ...

n **Think about the new Exo Earth?**

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**Conclusion**

n **Galvanizing on Earth is a Must**

- Ø Oxidizing atmosphere has more advantages than drawbacks
- Ø Lower gravity has no real Benefits
- Ø Life would not be funny because of the difficulty to organize friendly Barbecues due to lack of Oxygen

**Take care of our Planet !**